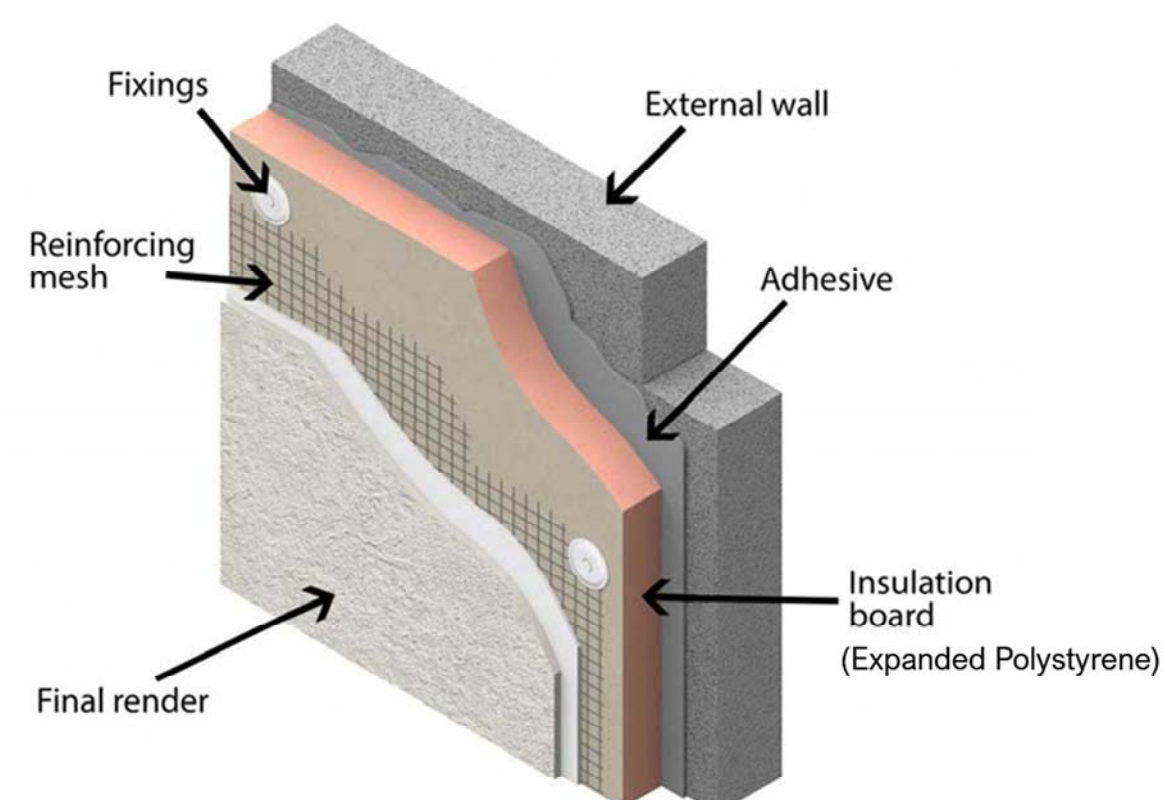


Introduction

In Europe, the external thermal insulation (ETI) has been developed extensively. However, this potentially translates into an increase in the fuel mass and fire propagation on the facade because the insulation materials are generally derived from plastic (PE, EPS, PIR, etc.).



| | |
|------------------|---------------------------|
| Insulation board | EPS |
| Fixing render | 68%Si, 14%Al, 9%Ca, 6%Mg |
| Final render | 53%Ca, 24%Si, 11%Al, 7%Ti |

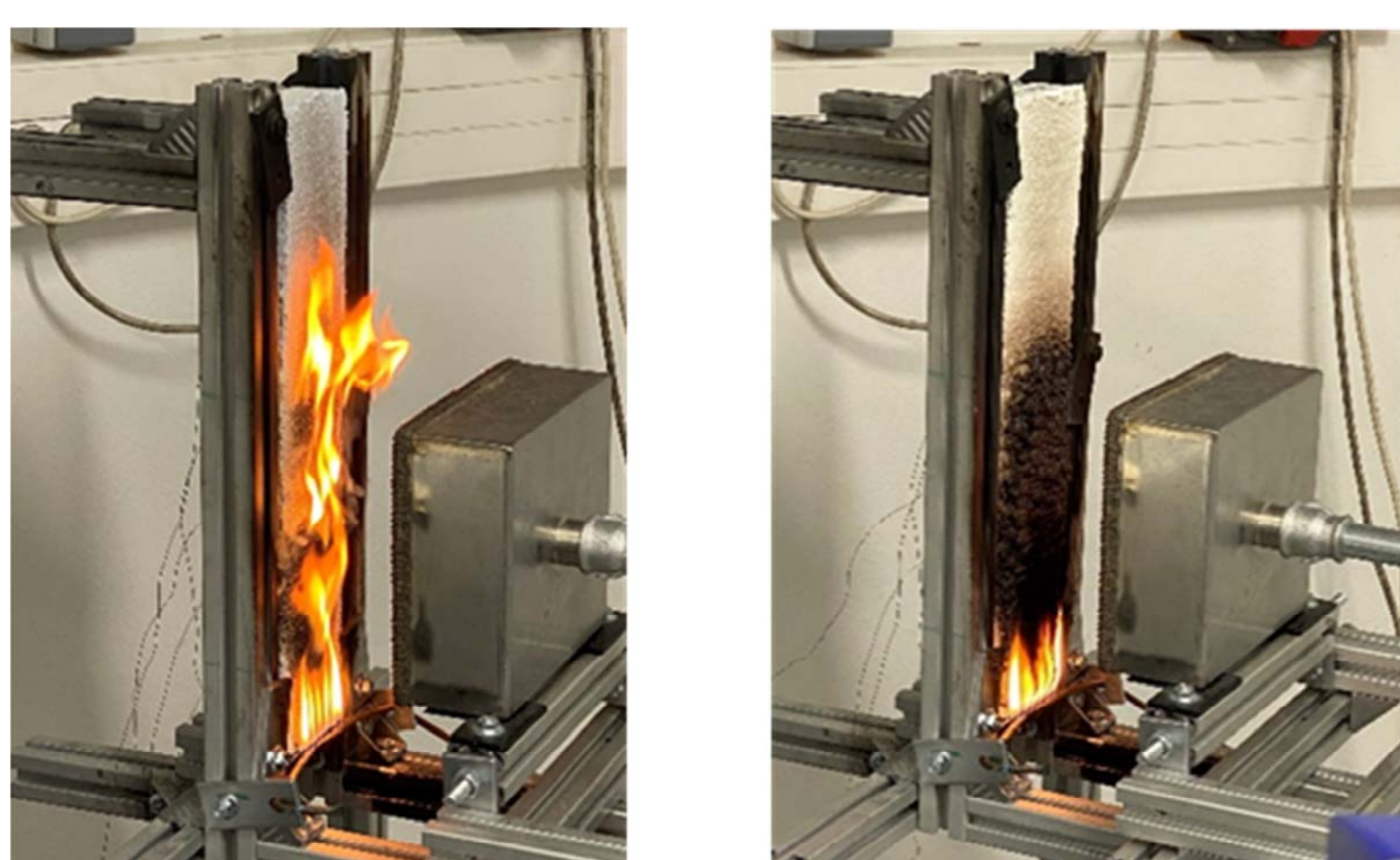
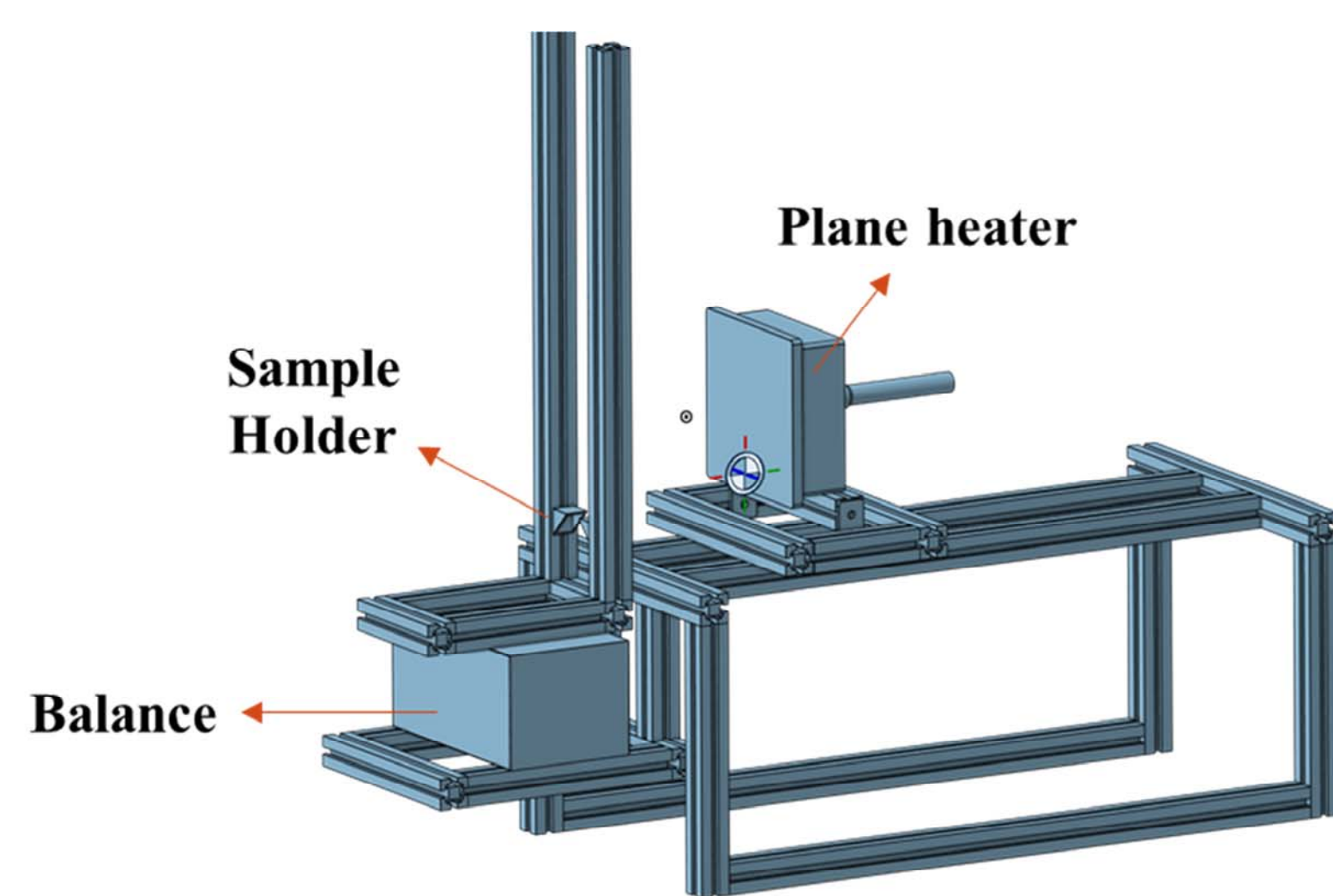
Objective

Describe the thermal decomposition process of ETI elements at small scale

Characterize the flame-facade interaction and propagation at intermediate-scale

Study some intumescent coating configurations for the fire protection of the facade at larger scale

Test Bench



A prototype by combining a plane radiant heater with a horizontal and rotational motion

Conclusion

An original test bench at intermediate scale is introduced, equipped with a plane radiant heater movable horizontally and rotationally, to study the thermal decomposition and the flame propagation. The new insulation coating by adding FlameOFF or Expandable Graphite works well in heat protection.

With kinetic parameters of reaction investigated by TGA, like reaction order, activation energy and pre-exponential factor, it is possible to define the rate of decomposition of ETI materials as a function by using Arrhenius law. Then, the heat of gasification and decomposition could be evaluated from STA. Based on these parameters, a pyrolysis model was built, which contribute to understanding the observed phenomena.

Results

TGA

| EPS | |
|---------------|-----------------|
| E_a | 177,619 kJ/mol |
| $Log(PreExp)$ | 11,996 Log(1/s) |
| n | 1,184 |
| θ | 1,004 |

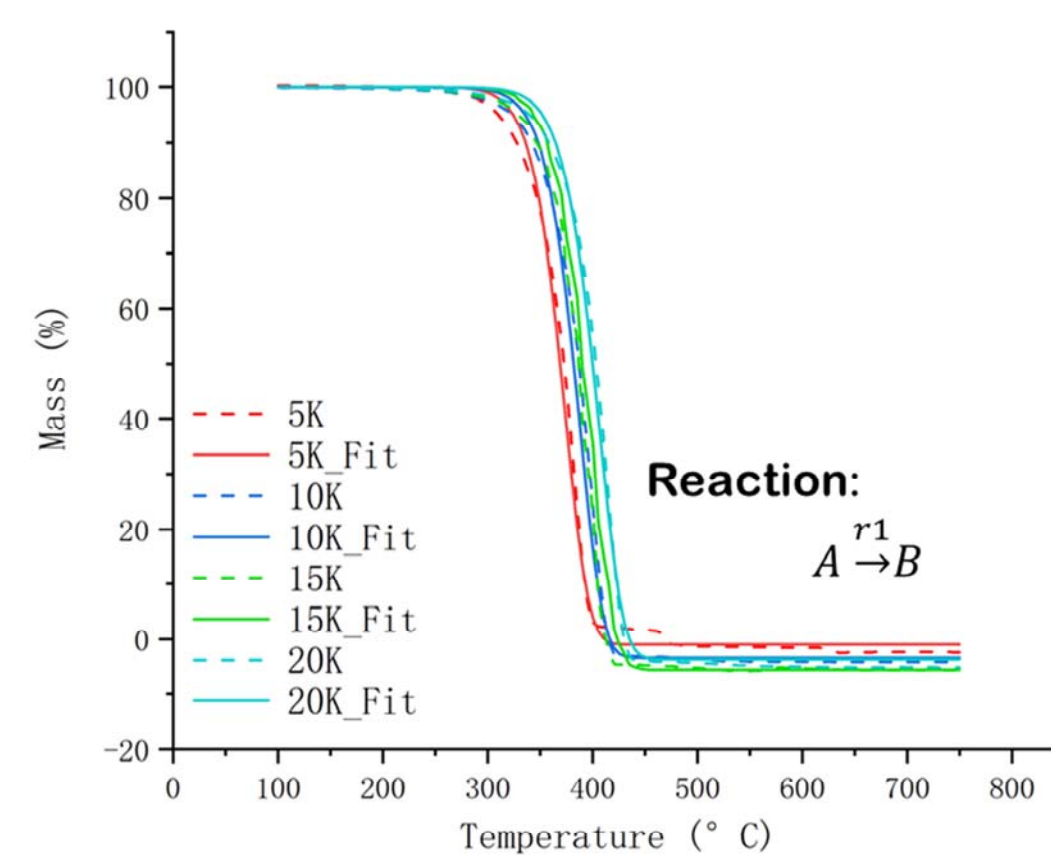


Fig.1 TG fit curves of EPS in air

| Finition | Step1 | Step2 |
|-----------------------|----------------|-----------------|
| E_a | 79,901 kJ/mol | 356,130 kJ/mol |
| $\log(\text{PreExp})$ | 4,988 Log(1/s) | 16,782 Log(1/s) |
| n | 2,491 | 2,252 |
| θ | 0,463 | 0,536 |

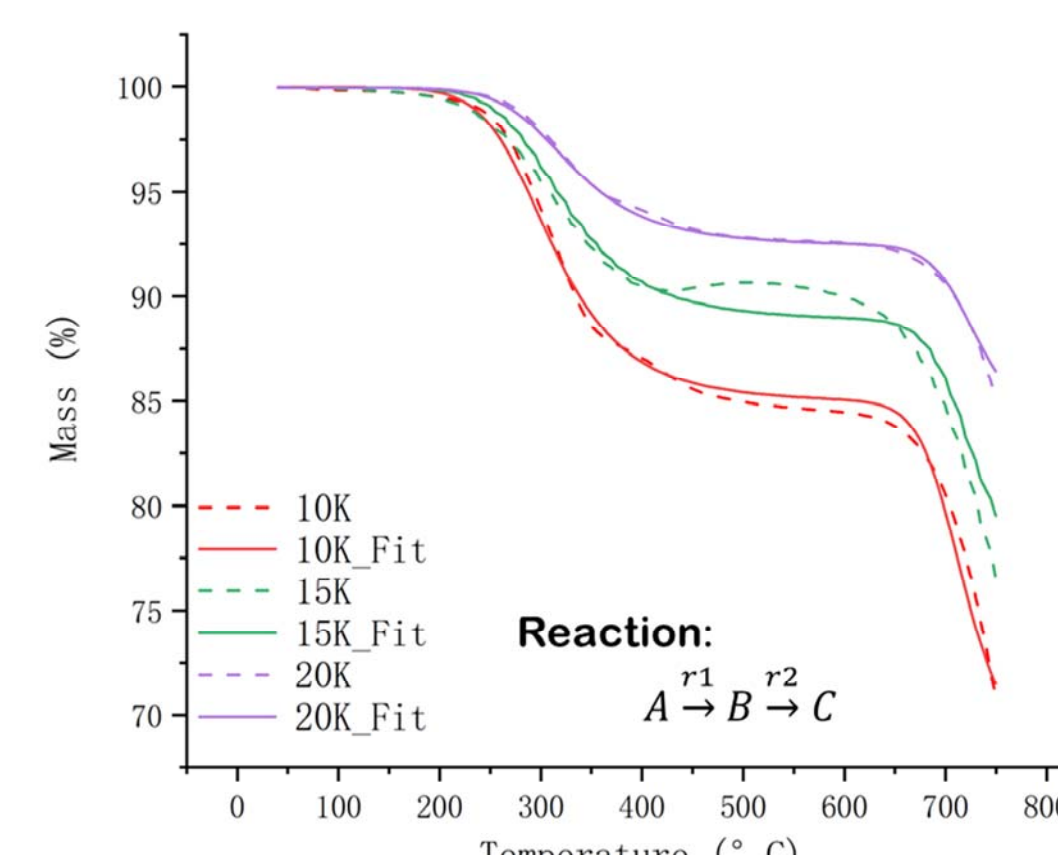


Fig.2 TG fit curves of final render in air

| FlameOFF | Final render + EG |
|--------------|-------------------|
| Final render | First render |
| First render | EPS |
| EPS | Cement board |
| Cement board | |

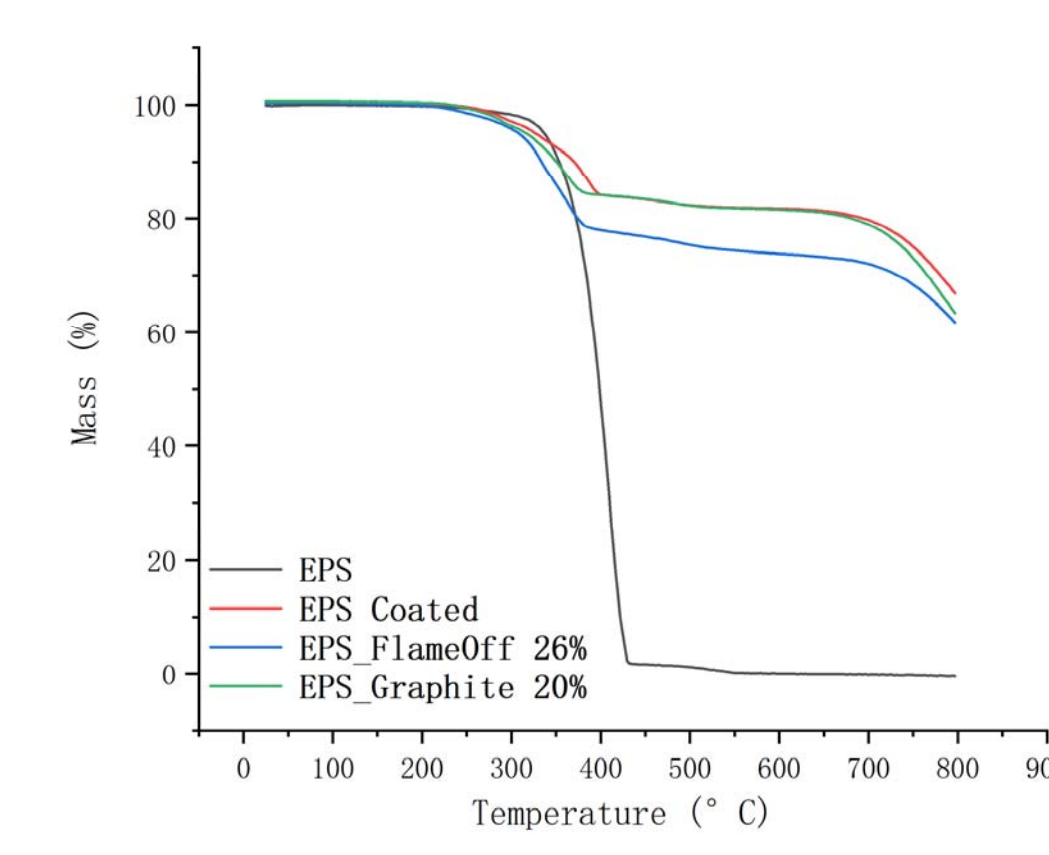


Fig.3 TG curves of different ETI in 10K/min in air

STA

| Step | Enthalpy (J/g) | Onset Temperature(°C) | Mass Loss(%) |
|------|----------------|-----------------------|--------------|
| M | 160.8 | $T_i = 44$ | - |
| | | $T_i = 125$ | |
| 1 | -603.1 | 387.3 | 98.22 |

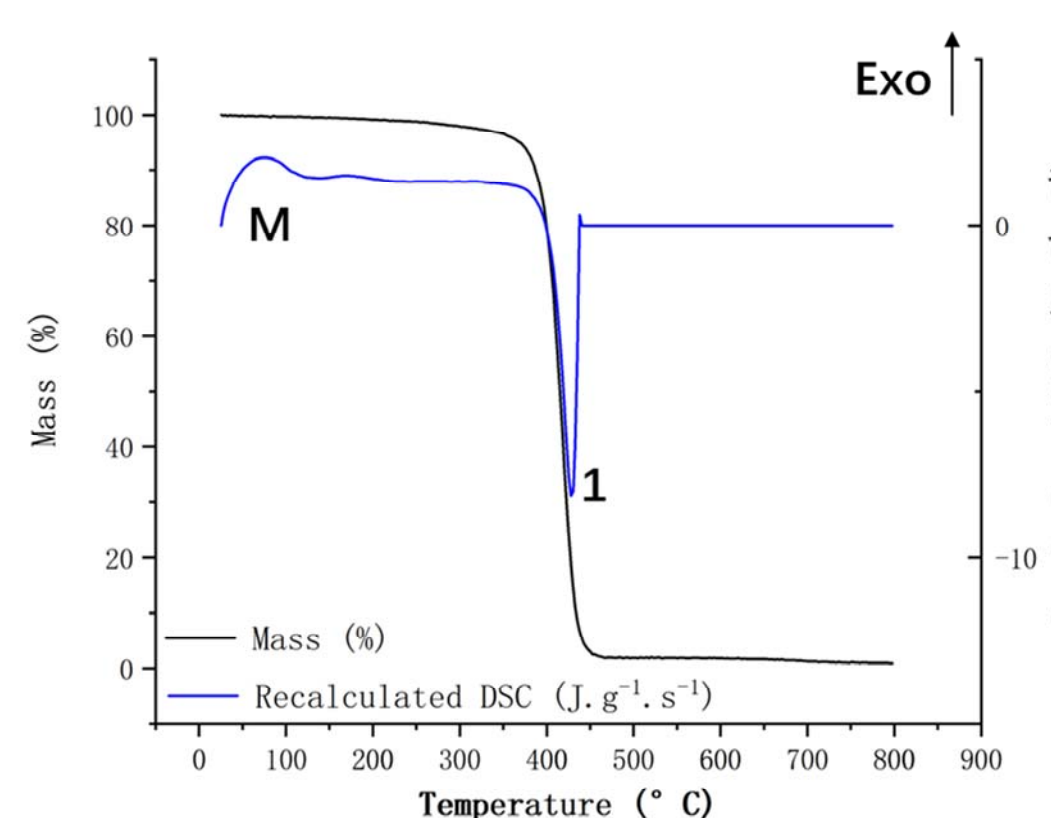


Fig.4 STA curves of EPS in 10K/min in nitrogen

| Step | Enthalpy (J/g) | Onset Temperature(°C) | Mass Loss(%) |
|------|----------------|-----------------------|--------------|
| 1 | -418,113 | 318,9 | 99,98 |

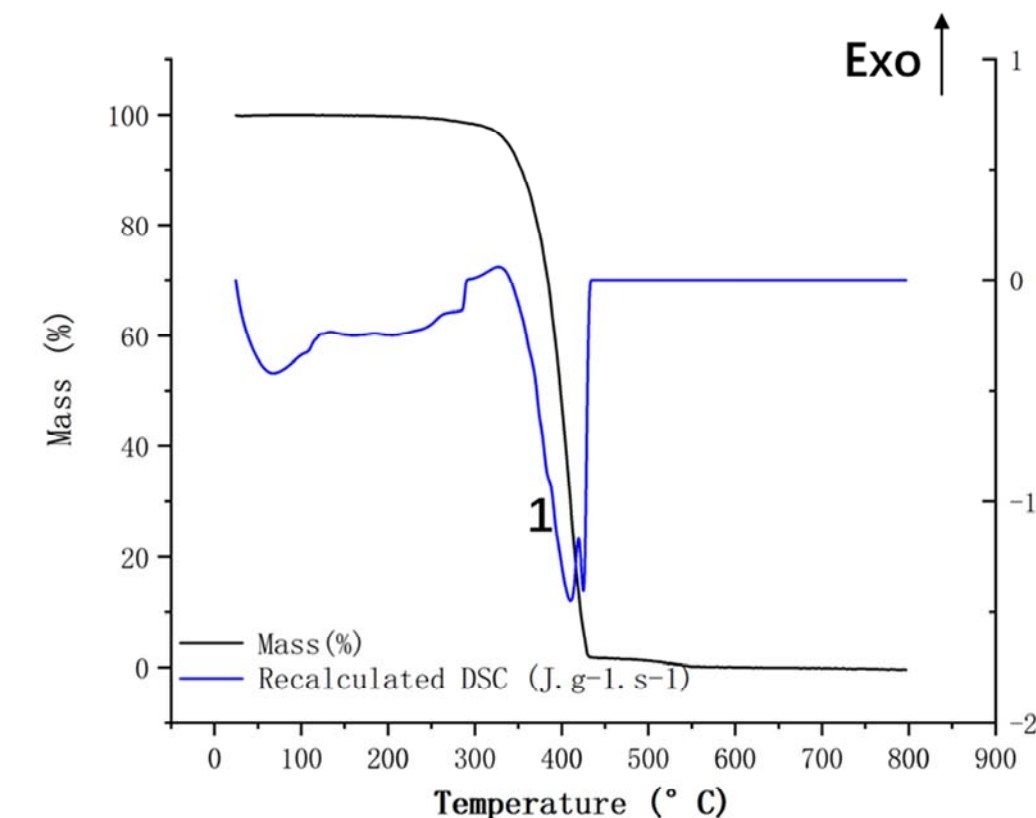


Fig.5 STA curves of EPS in 10K/min in air

| Step | Enthalpy (J/g) | Onset Temperature(°C) | Mass Loss(%) |
|------|----------------|-----------------------|--------------|
| 1 | -98.48 | 184 | 6.17 |
| 2 | -82.16 | 395.7 | 15.56 |
| 3 | -438.8 | 750.1 | 16.37 |

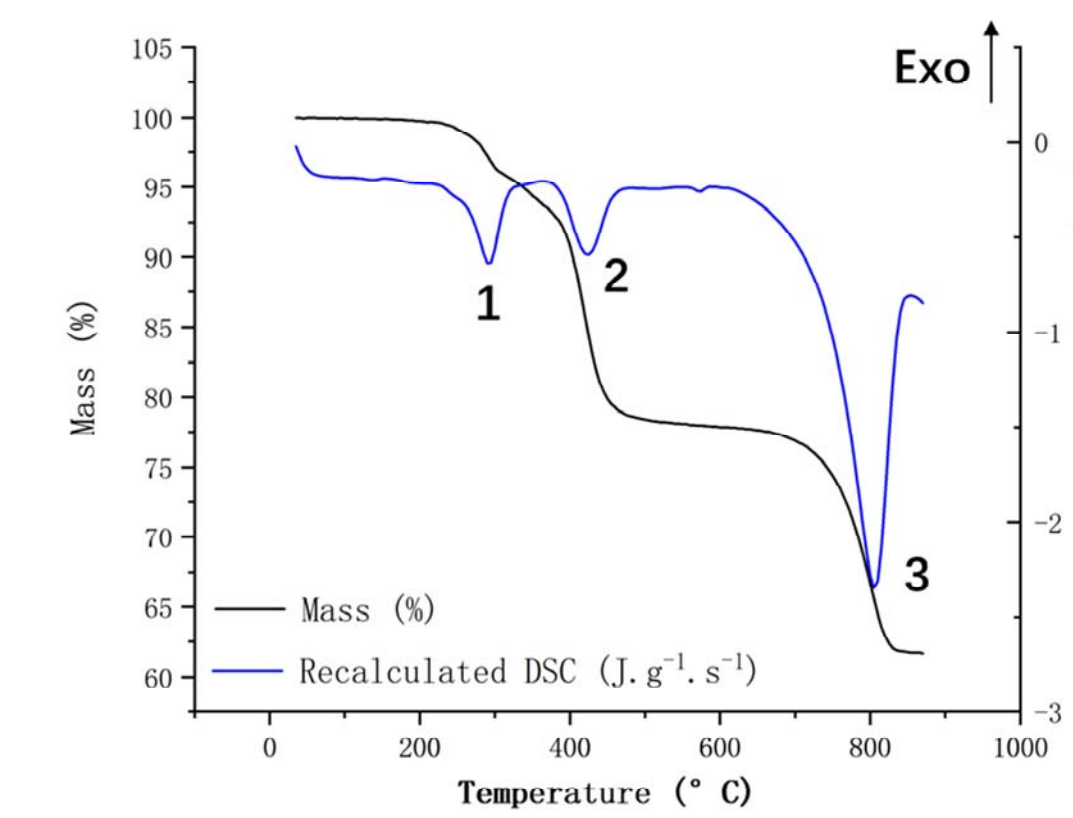


Fig.6 STA curves of ETI in 10K/min in nitrogen

Temperature Profile

Condition: Plane heater 10cm, 0° no incline, 60 kW/m²

| |
|--------------|
| Final render |
| First render |
| EPS |
| Cement board |

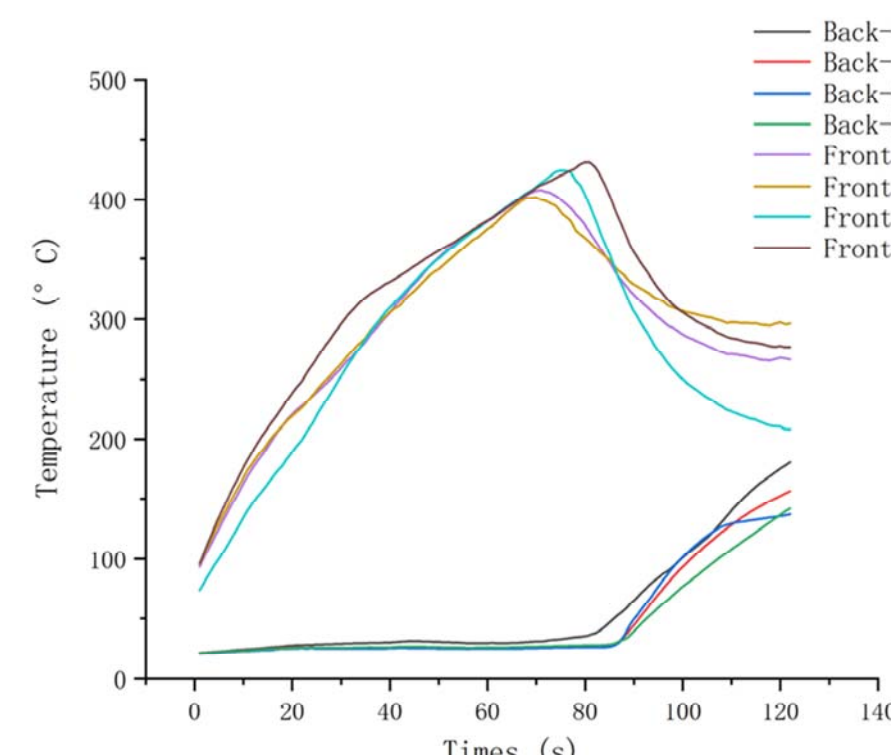


Fig.7 Temperature curves of commercial ETI

| |
|--------------|
| FlameOFF |
| Final render |
| First render |
| EPS |
| Cement board |

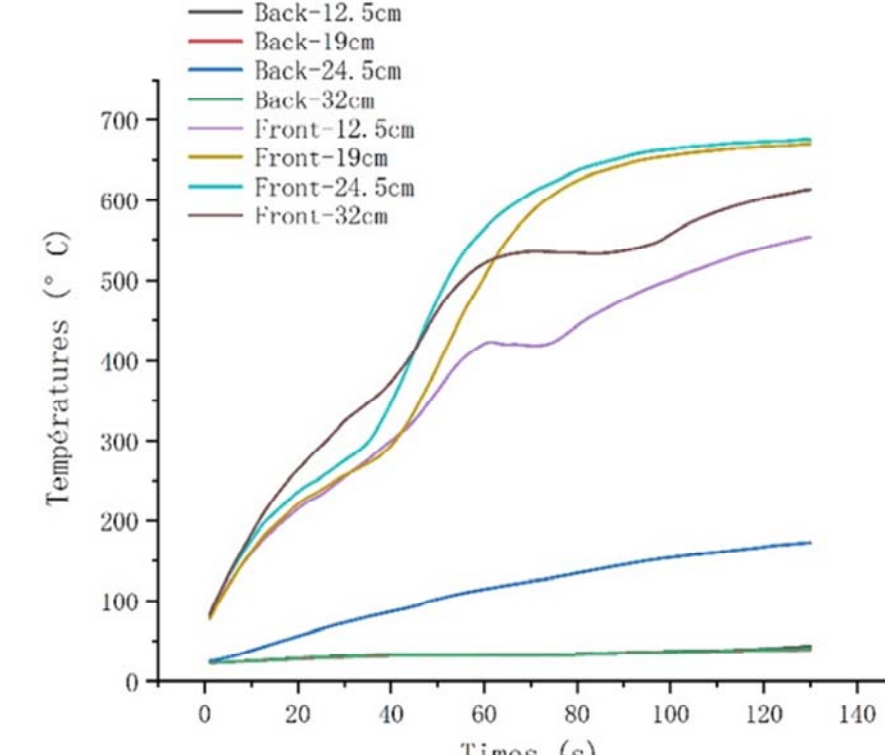


Fig.8 Temperature curves of ETI + FlameOFF

| |
|-------------------|
| Final render + EG |
| First render |
| EPS |
| Cement board |

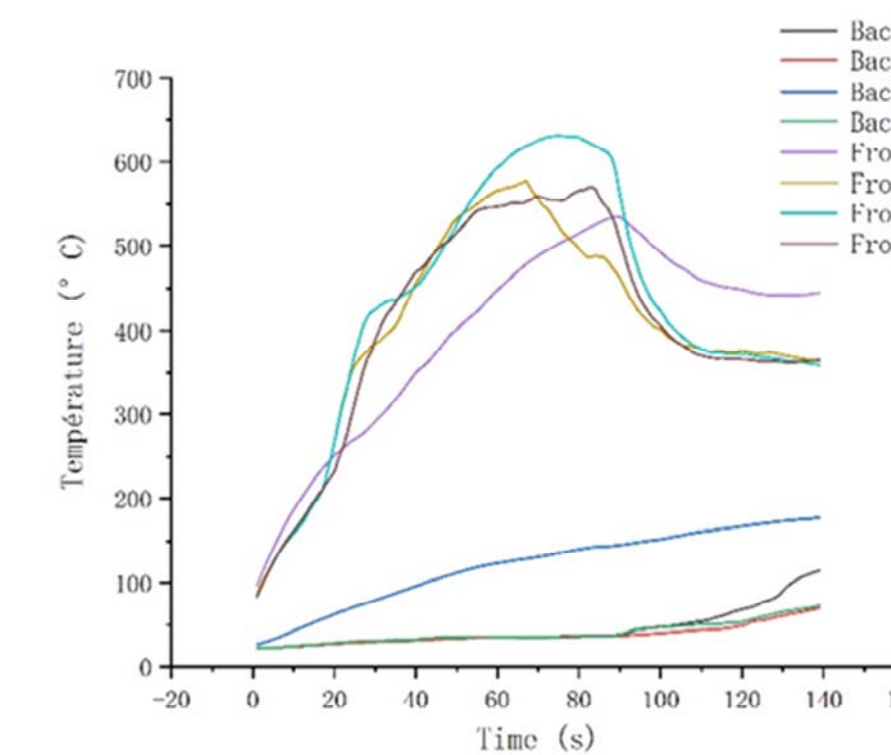


Fig.9 Temperature curves of ETI + EG

Simulation- EPS degradation

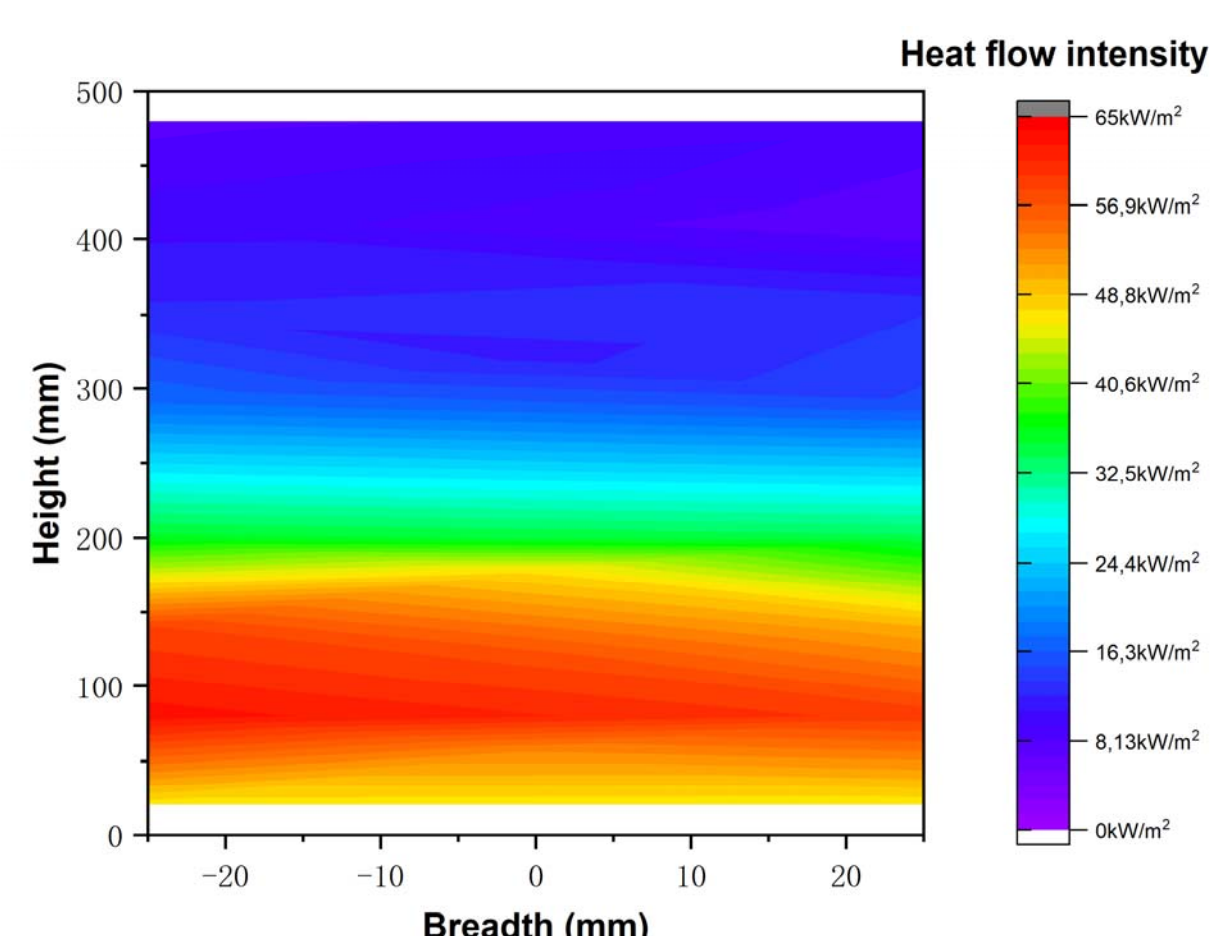


Fig.10 Distribution of heat flux on facade

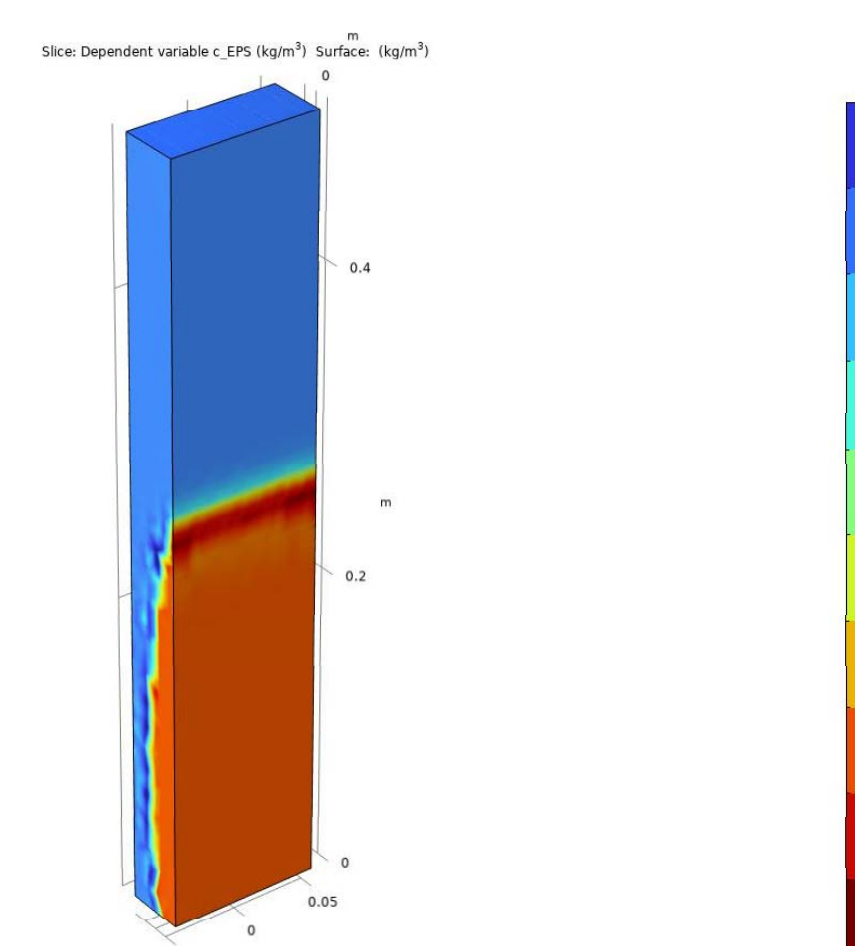


Fig.11 Simulated EPS Concentration at 200s

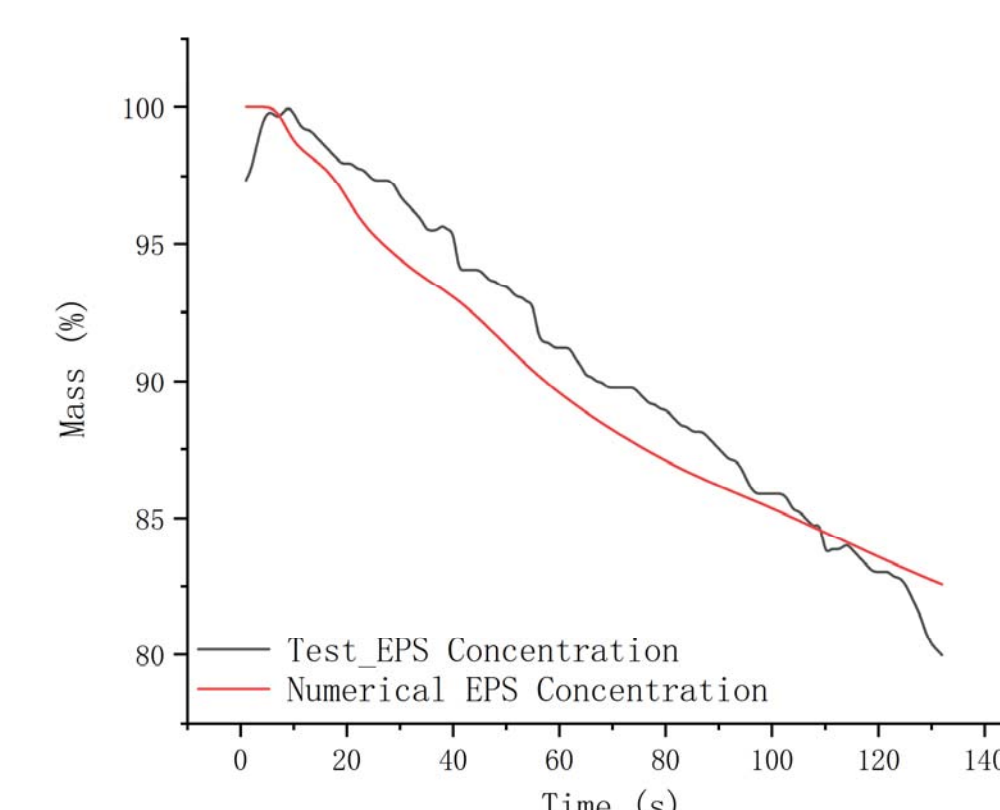


Fig.12 Comparison of mass loss